

Lecture 8

Terrestrial infrared radiative processes. Part 4:

Infrared radiative transfer in the plane-parallel atmosphere.

IR radiative heating/cooling rates

Objectives:

1. Infrared radiative transfer in the plane-parallel atmosphere.
2. Infrared radiative heating/cooling rates.
3. Concept of broadband flux emissivity.

Required reading:

L80: 1.4.4; 4.3; 4.7; 4.8.1

Recommended/advanced reading:

Le93:11 G&Y: 6.3-6.4

1. Infrared radiative transfer in the plane-parallel atmosphere.

- Recall Lecture 6 where we have derived the solutions of a radiative transfer for the **monochromatic upward and downward intensities** in the IR for a plane-parallel atmosphere consisting of absorbing gases (no scattering => no clouds, no aerosols) (see Eq.[6.3a, b] and Eq.[6.4a, b]).

$$I_n^\uparrow(t; \mathbf{m}) = B_n(t^*) \exp\left(-\frac{t^* - t}{\mathbf{m}}\right) + \frac{1}{\mathbf{m}} \int_t^{t^*} \exp\left(-\frac{t' - t}{\mathbf{m}}\right) B_n(t') dt' \quad [6.3a]$$

$$I_n^\downarrow(t; -\mathbf{m}) = \frac{1}{\mathbf{m}} \int_0^t \exp\left(-\frac{t - t'}{\mathbf{m}}\right) B_n(t') dt' \quad [6.3b]$$

and

$$I_n^\uparrow(t; \mathbf{m}) = B_n(t^*) T_n((t^* - t) / \mathbf{m}) - \int_t^{t^*} B_n(t') \frac{dT_n((t' - t) / \mathbf{m})}{dt'} dt' \quad [6.4a]$$

$$I_n^\downarrow(t; -\mathbf{m}) = \int_0^t B_n(t') \frac{dT_n((t - t') / \mathbf{m})}{dt'} dt' \quad [6.4b]$$

Recall that Eq.[6.3a, b] and Eq.[6.4a, b] have been derived the whole atmosphere with the optical depth τ_v^* assuming two boundary conditions:

Surface: assumed to be a blackbody in the IR emitting with the surface temperature T_s ,

$$I_n^\uparrow(\mathbf{t}_n^*, \mathbf{m}) = B_n(T_s) = B_n(T_s(\mathbf{t}_n^*)) = B_n(\mathbf{t}_n^*)$$

Top of the atmosphere (TOA), $t_n = 0$: no downward emission

$$I_n^\downarrow(0, \mathbf{m}) = B_n(TOA) = 0$$

- For various practical applications we need to know the radiative flux (or irradiance).

We can introduce the **monochromatic upward and downward fluxes** by using the general definition for a monochromatic radiative flux (see Lecture 2, Eq.[2.6])

$$F_l = \int_{\Omega} I_l \cos(\mathbf{q}) d\Omega \quad [2.6]$$

and that $d\Omega = \sin(\mathbf{q}) d\mathbf{q} d\mathbf{j}$

Therefore we have

$$\begin{aligned}
 F_n^\uparrow &= \int_0^{2p} \int_0^{p/2} I_n^\uparrow(\mathbf{q}; \mathbf{j}) \cos(\mathbf{q}) \sin(\mathbf{q}) d\mathbf{q} d\mathbf{j} = \\
 &= -2p \int_0^{p/2} I_n^\uparrow(\mathbf{q}) \cos(\mathbf{q}) d(\cos(\mathbf{q})) = \\
 &= 2p \int_0^1 I_n^\uparrow(\mathbf{m}) \mathbf{m} d\mathbf{m}
 \end{aligned}$$

NOTE: above we assumed that there is no dependency of \mathbf{f} in the plane-parallel atmosphere. Also we used that $d(\cos q) = -\sin(q) dq$

Performing the similar derivation for F_n^\downarrow , we have

$$\begin{aligned}
 F_n^\uparrow &= 2p \int_0^1 I_n^\uparrow(\mathbf{m}) \mathbf{m} d\mathbf{m} \\
 F_n^\downarrow &= 2p \int_0^1 I_n^\downarrow(-\mathbf{m}) \mathbf{m} d\mathbf{m}
 \end{aligned}
 \tag{8.1}$$

Thus we can re-write the radiative transfer equation and its solution (Eq.[6.1a, b] and Eq.[6.3a, b]) in terms of **the monochromatic upward and downward fluxes**.

Similar to Eq.[6.3a, b] we have

$$\begin{aligned}
 F_n^\uparrow(t) &= 2pB_n(t^*) \int_0^1 \exp\left(-\frac{t^* - t}{m}\right) m dm \\
 &+ 2p \int_0^1 \int_t^{t^*} \exp\left(-\frac{t' - t}{m}\right) B_n(t') dt' dm
 \end{aligned}
 \tag{8.2a}$$

and

$$F_n^\downarrow(t) = 2p \int_0^1 \int_0^t \exp\left(-\frac{t - t'}{m}\right) B_n(t') dt' dm
 \tag{8.2b}$$

- To integrate Eq.[8.2a, b] over m, let's introduce the **exponential integral** defined as

$$E_n(t) = \int_1^\infty \frac{\exp(-tx)}{x^n} dx$$

NOTE:

$$\frac{dE_n(t)}{dt} = -\int_1^\infty \frac{\exp(-tx)}{x^n} dx = -E_{n-1}(t)$$

Also note that

$$E_3(t^* - t) = \int_1^\infty \frac{\exp(-(t^* - t)x)}{x^3} dx ;$$

$$E_2(t^* - t) = \int_1^\infty \frac{\exp(-(t^* - t)x)}{x^2} dx$$

Let's make the following substitutions in Eq.[8.2a, b]: $x = 1/m$, hence $d\mu = -dx/x^2$. Thus, the integral in the first term on the right side in Eq.[8.2a] is

$$\int_0^1 \exp\left(-\frac{t^* - t}{m}\right) m dm = \int_1^\infty \exp(-(t^* - t)x) \frac{1}{x} \frac{dx}{x^2} = E_3(t^* - t)$$

and the integral in the second term on the right side in Eq.[8.2a] (which is the same as the integral in Eq.[8.2b]) is

$$\int_0^1 \exp\left(-\frac{t^* - t}{m}\right) dm = \int_1^\infty \exp(-(t^* - t)x) \frac{dx}{x^2} = E_2(t^* - t)$$

Therefore, Eq.[8.2a,b] can be written as

$$F_n^\uparrow(t) = 2p B_n(t^*) E_3(t^* - t) + 2p \int_t^{t^*} E_2(t' - t) B_n(t') dt' \quad [8.3a]$$

$$F_n^\downarrow(t) = 2p \int_0^t E_2(t - t') B_n(t') dt' \quad [8.3b]$$

- **Eq.[8.3a, b] is a final solution for infrared monochromatic fluxes** in the plane-parallel gaseous atmosphere.

NOTE: The **exponential integral** E_n cannot be analytically integrated but it can be pre-calculated using existing programs without any serious difficulties.

- **Line-by-line code** provides an “exact” solution of Eq. [8.3a, b] (recall Lecture 6)

Recall that the **total (integral) flux** is defined as $F(\mathbf{t}) = \int F_n(\mathbf{t}) d\mathbf{n}$

Thus, we obtain the total (integral) upward and downward fluxes in the plane-parallel atmosphere by integrating Eq.[8.3a, b] over the entire infrared spectrum,

$$F^\uparrow(\mathbf{t}) = 2p \int_0^\infty B_n(\mathbf{t}^*) E_3(\mathbf{t}^* - \mathbf{t}) d\mathbf{n} + 2p \int_0^\infty \int_t^{\mathbf{t}^*} E_2(\mathbf{t}' - \mathbf{t}) B_n(\mathbf{t}') dt' d\mathbf{n} \quad [8.4a]$$

$$F^\downarrow(\mathbf{t}) = 2p \int_0^\infty \int_0^{\mathbf{t}} E_2(\mathbf{t} - \mathbf{t}') B_n(\mathbf{t}') dt' d\mathbf{n} \quad [8.4b]$$

Let's introduce **the transmission function** for the radiative flux (called **diffuse transmission function** or **slab transmission function**).

Monochromatic diffuse transmission function (or transmittance):

$$T_n^f(\mathbf{t}) = 2 \int_0^1 T_n(\mathbf{t} / \mathbf{m}) m dm \quad [8.5]$$

where $T_n(\mathbf{t}/\mathbf{m})$ is the monochromatic transmittance defined in Lecture 5, part 3.

NOTE: $T_n(\mathbf{t}/\mathbf{m})$ gives the attenuation of intensity passing a layer with the optical depth \mathbf{t} .

Spectral diffuse transmission function (or transmittance):

$$T_{\bar{n}}^f(\mathbf{t}) = 2 \int_0^1 T_{\bar{n}}(\mathbf{t} / \mathbf{m}) m dm \quad [8.6]$$

Using the definition of a **monochromatic diffuse transmittance** and solution of the radiative transfer equation expressed via **the transmittance** Eq.[6.4a, b], the solution for fluxes can be written as

$$\begin{aligned}
 F_n^\uparrow(t) &= pB_n(t^*)T_n^f(t^* - t) \\
 &- \int_t^{t^*} pB_n(t') \frac{dT_n^f(t' - t)}{dt'} dt'
 \end{aligned}
 \tag{8.7a}$$

and

$$F_n^\downarrow(t) = \int_0^t pB_n(t') \frac{dT_n^f(t - t')}{dt'} dt'
 \tag{8.7b}$$

NOTE: On the right side of Eq.[8.7a] for the upward flux, the first term gives the surface emission that is attenuated to the level t and the second term gives the emission from the atmospheric layers characterized by the Planck function multiplied by the **weighting function** dT_n^f / dt . Likewise, the downward flux at a given layer (Eq.[8.7b]) is produced by the emission from the atmospheric layers.

2. Infrared radiative heating/cooling rates.

- Radiative processes may affect the dynamics and thermodynamics of the atmosphere through the generation of **radiative heating/cooling rates**.

NOTE: The thermodynamic equation for the temperature changes in the atmosphere (i.e. the first law of thermodynamic for moist air) includes **the radiative energy exchange term (i.e. total radiative heating/cooling rates** which are solar plus infrared heating/cooling rates). In this lecture we discuss IR radiative rates only (solar will be discussed later in the course).

Let's introduce the **monochromatic net flux** at a given height defined as

$$F_n(z) = F_n^\uparrow(z) - F_n^\downarrow(z)$$

Also we can define total **net flux**:

$$F(z) = F^\uparrow(z) - F^\downarrow(z)$$

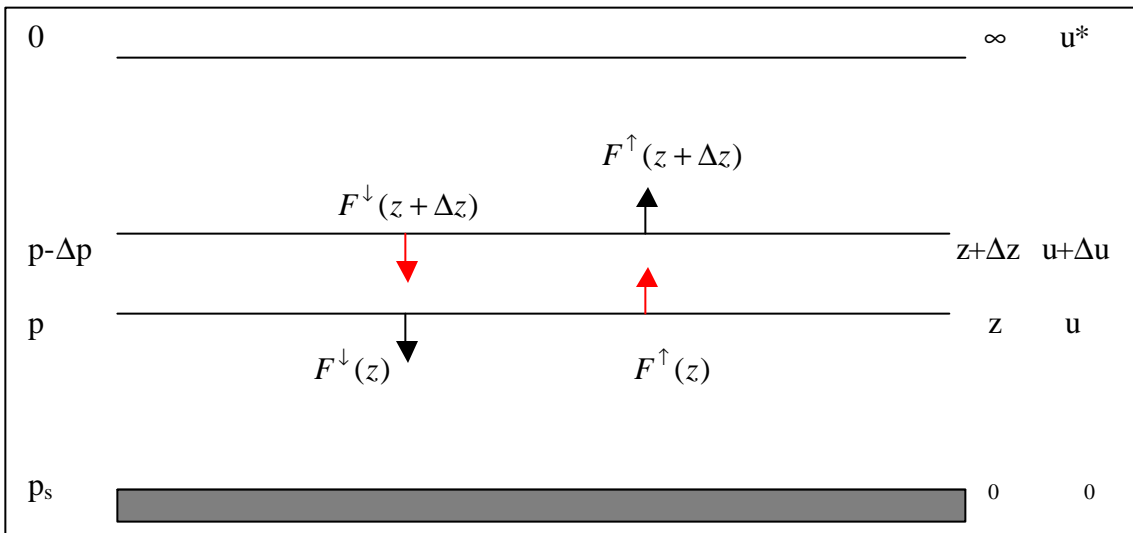
Introducing the net flux $F(\mathbf{z}+D\mathbf{z})$ at the level $\mathbf{z}+D\mathbf{z}$, we find the **net flux divergence** for the layer $D\mathbf{z}$ is

$$\Delta F = F(z + \Delta z) - F(z)$$

NOTE: The **net flux divergence** gives the radiative gain by a layer due to absorption or lost by a layer due to the emission, depending on a sign of ΔF .

$F(\mathbf{z}+D\mathbf{z}) < F(\mathbf{z})$ (hence $\Delta F < 0$) \Rightarrow a layer gains radiative energy \Rightarrow heating

$F(\mathbf{z}+D\mathbf{z}) > F(\mathbf{z})$ (hence $\Delta F > 0$) \Rightarrow a layer losses radiative energy \Rightarrow cooling



The IR **radiative heating (or cooling) rate** is defined as the rate of temperature change of the layer dz due to IR radiative energy gain (or loss):

$$\left(\frac{\partial T}{\partial t} \right)_{IR} = \int_0^{\infty} \left(\frac{\partial T}{\partial t} \right)_n dv = - \frac{1}{c_p \mathbf{r}} \frac{dF(z)}{dz} \quad [8.8]$$

where c_p is the specific heat at the constant pressure ($c_p = 1004.67 \text{ J/kg/K}$) and r is the air density in a given layer.

Heating /cooling radiative rates may be expressed in pressure coordinates:

From hydrostatic equation (see Lecture 4) we have

$$dp = -r g dz$$

with $g = 9.806 \text{ m/s}^2$ is gravitational acceleration.

Using $dz = - dp/r g$, we have

$$\left(\frac{\partial T}{\partial t} \right)_{IR} = \frac{g}{c_p} \frac{dF(z)}{dp} \quad [8.9]$$

NOTE: g/c_p is the adiabatic lapse rate.

NOTE: Lab 5 is devoted to the detail modeling of the IR radiative heating rates in the gaseous atmosphere.

3. Concept of broadband flux emissivity

- The **broadband flux emissivity** approach allows calculation of infrared fluxes and heating/cooling rates utilizing the temperature in terms of the Stefan-Boltzmann law instead of the Planck function.

Based on Eq.[8.7 a, b], the total upward and downward fluxes in the path length u coordinates may be expressed as

$$F^{\uparrow}(u) = \int_0^{\infty} \mathbf{p} B_n(T_s) T_n^f(u) d\mathbf{n} + \int_0^{\infty} \int_0^u \mathbf{p} B_n(T(u')) \frac{dT_n^f(u-u')}{du'} du' d\mathbf{n} \quad [8.10a]$$

and

$$F^{\downarrow}(u) = \int_0^{\infty} \int_{u^*}^u \mathbf{p} B_n(T(u')) \frac{dT_n^f(u'-u)}{du'} du' d\mathbf{n} \quad [8.10b]$$

From the Stefan-Boltzmann law (see Lecture 3), we have

$$\int_0^{\infty} \mathbf{p} B_n(T) d\mathbf{n} = \mathbf{s}_B T^4$$

Let's define **the isothermal broadband emissivity** as

$$\mathbf{e}^f(u, T) = \frac{\int_0^{\infty} \mathbf{p} B_n(T) (1 - T_n^f(u)) d\mathbf{n}}{\mathbf{s}_B T^4} \quad [8.11]$$

Using the **isothermal broadband emissivity**, it can be shown (see L92: 2.7.2) that Eq.[8.10a, b] may be approximated as

$$F^{\uparrow}(u) \cong \mathbf{s}_B T_s^4 (1 - \mathbf{e}^f(u, T_s)) - \int_0^u \mathbf{s}_B T^4(u') \frac{d\mathbf{e}^f(u - u', T(u'))}{du} du' \quad [8.12a]$$

and

$$F^{\downarrow}(u) \cong \int_u^{u^*} \mathbf{s}_B T^4(u') \frac{d\mathbf{e}^f(u' - u, T(u'))}{du'} du' \quad [8.12b]$$

NOTE: If the **isothermal broadband emissivity** is known, the broadband fluxes and heating/cooling rates can be easily calculated from Eq.[8.12a, b].

NOTE: There are various parameterizations of the **isothermal broadband emissivity** to account for IR absorption by atmospheric gases (e.g., see L92: 2.7.3).